

Article

# Bio-Kinetics of Simultaneous Nitrification and Aerobic Denitrification (SNaD) by a Cyanide-Degrading Bacterium Under Cyanide-Laden Conditions

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**Abstract:** A microorganism isolated and identified as *Acinetobacter courvalinii* was found to be able to perform sequential free cyanide (CN<sup>-</sup>) degradation, simultaneous nitrification and aerobic denitrification (SNaD); this ability was associated with the multiphase growth profile of the microorganism when provided with multiple nitrogenous sources. The effect of CN<sup>-</sup> on SNaD including enzyme expression, activity and protein functionality of *Acinetobacter courvalinii* was investigated. It was found that CN<sup>-</sup> concentration of 1.9 to 5.8 mg CN<sup>-</sup>/L did not affect the growth of *Acinetobacter courvalinii*. Furthermore, the degradation rates of CN<sup>-</sup> and ammonium-nitrogen (NH<sub>4</sub>-N) were found to be 2.2 mg CN<sup>-</sup>/L/h and 0.40 mg NH<sub>4</sub>-N/L/h, respectively. Moreover, five models' (Monod, Moser, Generic Rate law, Haldane, and Andrews) ability to predict SNaD under CN<sup>-</sup> conditions, indicated that, only the Rate law, Haldane and Andrew's models, were suited to predict both SNaD and CN<sup>-</sup> degradation. The effect of CN<sup>-</sup> on NH<sub>4</sub>-N, nitrate-nitrogen (NO<sub>3</sub><sup>-</sup>) and nitrite-nitrogen (NO<sub>2</sub><sup>-</sup>) oxidizing enzymes indicated that the CN<sup>-</sup> did not affect the expression and activity of ammonia monooxygenase (AMO); albeit, reduced the expression and activity of nitrate reductase (NaR) and nitrite reductase (NiR). Nevertheless, a slow decrease in NO<sub>2</sub><sup>-</sup> was observed after the supplementation of CN<sup>-</sup> to the cultures, thus confirming the activity of NaR and the activation of the denitrification pathway by the CN<sup>-</sup>. These special characteristics of the *Acinetobacter courvalinii* isolate, suggests its suitability for the treatment of wastewater containing multiple nitrogenous compounds in which CN<sup>-</sup> is present.

**Keywords:** aerobic denitrification; bio-kinetics; free cyanide; nitrate-nitrogen; nitrification; nitrite-nitrogen

## 1. Introduction

Untreated total nitrogen (TN)-containing wastewater in the environment can result in eutrophication, thus the treatment of such wastewater containing TN is crucial in wastewater treatment

plants (WWTPs) [1]. This type of wastewater may be treated by either physicochemical or biological methods. Most municipal and industrial wastewater treatment plants use biological methods such as simultaneous nitrification and aerobic denitrification (SNaD) for the treatment of contaminated water due to the cost-effectiveness of such processes [2,3].

However, SNaD is sensitive to toxicant loading [4–6], particularly free cyanide ( $\text{CN}^-$ ) [5]. Physical and chemical methods have been used to reduce  $\text{CN}^-$  effects on SNaD; however, these methods are relatively expensive, complex and produce undesirable by-products such as hypochlorite, and toxicant loaded sludge [7]. Hence, biological removal of  $\text{CN}^-$  prior to SNaD has recently received the most attention. Biological  $\text{CN}^-$  removal has been proven to be an ideal option because of its cost effectiveness and environmental benignity [8]. Although, biological  $\text{CN}^-$  removal reduces the production of undesirable by-products, conducting  $\text{CN}^-$  degradation in a separate reactor with SNaD in sequential two stage reactor systems, may result in the escalation of costs associated with the operation of the multiple independent reactors dedicated to the biodegradation of  $\text{CN}^-$  and TN. Han et al. [9] proposed that  $\text{CN}^-$  degrading and resistant microorganisms can be used for SNaD in order to lower the inhibition effect of  $\text{CN}^-$  towards SNaD in a single reactor system.

Mekuto et al. [10] reported that *Bacillus* species were capable of degrading up to 300 mg  $\text{CN}^-$ /L and subsequently utilize the by-products which were  $\text{NH}_4\text{-N}$ ,  $\text{NO}_3\text{-N}$  and  $\text{NO}_2\text{-N}$ . Additionally, Mpongwana et al. [11] isolated a  $\text{CN}^-$  tolerant strain capable of simultaneous  $\text{CN}^-$  degradation and SNaD. However, the applicability of  $\text{CN}^-$  degrading and resistant microorganisms is still restricted due to the lack of information necessary to adequately control SNaD under high  $\text{CN}^-$  loading conditions. Hence, this paper reports on the isolation of an organism that simultaneously degrades  $\text{CN}^-$  while performing SNaD, with the phenomena of simultaneous  $\text{CN}^-$  degradation and  $\text{NH}_4\text{-N}$  removal being modeled by the determination of kinetic parameters using numerous decay models. The mechanism by which  $\text{CN}^-$  affects the nitrification and denitrification enzymes is still not documented, thus making it difficult to apply  $\text{CN}^-$  resistant microorganisms in SNaD systems, in which  $\text{CN}^-$  laden wastewater is being treated. To also address this research gap, the expression and activity of ammonia monooxygenase (AMO), nitrate reductase (NaR) and nitrite reductase (NiR) present in the  $\text{CN}^-$  resistant isolates' supernatant, deemed suitable for this research, was also conducted.

## 2. Materials and Methods

### 2.1. Isolation and Identification of the Bacterial Isolate of Interest

The isolate used in this study was isolated from  $\text{CN}^-$  containing waste at the Bioresource Engineering Research Group (*BioERG*) laboratory, Cape Peninsula University of Technology, Cape Town, South Africa. This organism was sub-cultured to obtain pure colonies and subjected to toxicant ( $\text{CN}^-$ ) resistance testing to determine the highest  $\text{CN}^-$  concentration it can withstand subsequent to gram staining. The genomic DNA was extracted from the pure cultures using the Quick-DNA™, Fungal/Bacterial Miniprep kit, to target the 16S rRNA gene (Zymo Research, Irvine, CA, USA, Catalogue No. D6005). This region was amplified using the OneTaq® Quick-Load® 2X Master Mix (Zymo Research, Catalogue No. M0486) and the primers which were used were the 16S-27F and 16S-1492R with sequence (5' to 3') AGAGTTTGATCMTGGCTCAG, and CGGTTACCTTGTTACGACTT, respectively.

The PCR products were run on an agarose gel and the gel fragments were extracted using the Zymoclean™ Gel DNA Recovery Kit (Zymo Research, Catalogue No. D4001). The extracted fragments were sequenced in the forward and reverse direction using the Nimagen BrilliantDye™ Terminator Cycle Sequencing kit v3.1 and further purified using the Zymo Research, ZR-96 DNA Sequencing Clean-up kit™. The purified fragments were analyzed using the ABI 3500XL Genetic Analyzer (Applied Biosystems, ThermoFisher Scientific, Waltham, MA, USA). CLC Bio Main Workbench v7.6 was used to analyze the files generated by the ABI 3500XL Genetic Analyzer and results were obtained through a BLAST search (NCBI).

## 2.2. Batch Culture Experiments

A basal medium was used for SNaD and  $\text{CN}^-$  degradation studies. Erlenmeyer flasks (250 mL) were used with a working volume of 100 mL of basal media. The basal media was composed of: 1.5 g  $\text{KH}_2\text{PO}_4$ , 7.9 g  $\text{Na}_2\text{HPO}_4$ , 0.5 g  $\text{MgSO}_4 \cdot 7\text{H}_2\text{O}$ , and 1 mL of trace element solution per liter, was used. The trace element solution contained (per liter): 50 g EDTA, 2.2 g  $\text{ZnSO}_4 \cdot 7\text{H}_2\text{O}$ , 5.5 g  $\text{CaCl}_2$ , 5.06 g  $\text{MnCl}_2 \cdot 4\text{H}_2\text{O}$ , 5.0 g  $\text{FeSO}_4 \cdot 7\text{H}_2\text{O}$ , 1.1 g  $(\text{NH}_4)_6\text{Mo}_7\text{O}_{24} \cdot 4\text{H}_2\text{O}$ , 1.57 g  $\text{CuSO}_4 \cdot 5\text{H}_2\text{O}$ , 1.61 g  $\text{CoCl}_2 \cdot 6\text{H}_2\text{O}$ . The media was inoculated with a loop full of an overnight agar grown bacterial culture. The inoculated media was initially grown for 72 h without  $\text{NH}_4\text{-N}$  and  $\text{CN}^-$ , thereafter; 20 mg  $\text{NH}_4\text{-N/L}$  and 20 mg  $\text{CN}^-/\text{L}$  were added to the inoculated basal medium whereby samples were collected on a 24 h interval for 168 h to analyze  $\text{CN}^-$ ,  $\text{NH}_4\text{-N}$ ,  $\text{NO}_2^-$ ,  $\text{NO}_3^-$  and microbial growth at OD660 nm. The biomass concentration at OD660 nm was calculated by Equation (1) (from calibrated values in triplicate):

$$\text{OD660} = 0.0089 (\text{CFU}) - 0.3097 \quad (1)$$

## 2.3. Enzyme Extraction

To analyze the activities of the enzymes, i.e., AMO, NaR and NiR, cold acetone was added to the collected samples, forming a pellet that was separated from the supernatant by centrifuging each sample at 5000 g for 15 min. The pellet was lysed using a sonicator and the supernatant was collected by centrifugation at 16000 rpm for 5 min. Thereafter, the precipitate was washed three times and resuspended in phosphate (360 mg/L) buffer solution (pH 7.4).  $\text{NH}_4\text{-N}$  and  $\text{CN}^-$  solutions were prepared and the enzyme extracts were added into the  $\text{NH}_4\text{-N}$  and  $\text{CN}^-$  solutions, while the changes in  $\text{CN}^-$  (09701),  $\text{NH}_4\text{-N}$  (00683),  $\text{NO}_2\text{-N}$  (110057) and  $\text{NO}_3\text{-N}$  (14773) were monitored and analyzed using the Merck test kits (Merck Millipore., Burlington, USA).

The activity of the  $\text{NH}_4\text{-N}$  oxidizing enzyme was monitored by measuring the changes in  $\text{NH}_4\text{-N}$  after the addition of the enzyme extracts into the  $\text{NH}_4\text{-N}$  solution. The formation of  $\text{NO}_3\text{-N}$  from  $\text{NO}_2\text{-N}$  and the disappearance of  $\text{NO}_3\text{-N}$  were also monitored in order to determine the activity of both  $\text{NO}_3\text{-N}$  and  $\text{NO}_2\text{-N}$  oxidizing enzymes, i.e., NaR and NiR. The  $\text{CN}^-$  degrading enzymes were monitored with the changes in the concentration of  $\text{CN}^-$ .

## 2.4. Analytical Procedure(s)

All the test kits used for the analyses of the samples in this study were obtained from Merck SA a subsidiary of Merck Millipore., Burlington, USA. Furthermore, the Merck Spectroquant Nova 60 instrument was used to quantify the residual  $\text{CN}^-$ ,  $\text{NH}_4\text{-N}$ ,  $\text{NO}_2\text{-N}$ , and  $\text{NO}_3^-$  concentrations. The tests were conducted as per the manufacturer's instructions.

## 2.5. Kinetics Model Developed

During  $\text{CN}^-$  biodegradation, microorganisms convert  $\text{CN}^-$  to  $\text{NH}_4\text{-N}$  which was then used as a nitrogenous source. Mekuto et al. [10] reported the ability of cyanide degrading bacteria to degrade  $\text{CN}^-$  and subsequently utilize  $\text{NH}_4\text{-N}$ , with a further indication that some microorganisms are able to use  $\text{NH}_4\text{-N}$  and  $\text{CN}^-$  as nitrogenous sources simultaneously. It has been shown by Mpongwana et al. [11] that when a cyanide degrading microorganism is used for nitrification and denitrification under cyanide conditions, the microorganism undergoes, multiple growth phases, i.e., mostly diauxic growth; hence, growth models that describe diauxic growth must be considered when evaluating growth kinetic parameters of such microorganisms when removing TN. Multiphase growth rate was first described by Monod [12] as a sequential utilization of substrates accompanied by distinct exponential growth phases during a period in which the individual substrates were utilized.

In this study, Monod's and other models were also used to describe simultaneous  $\text{CN}^-$  degradation and SNaD, with all the experiments being carried out in a closed system (1L batch culture). The rate of toxicant pollutant degradation can be described as in Equation (2):

$$-\frac{dC_a}{dt} = r_a = K_i C_a^n \quad (2)$$

where  $r_a$  is the rate of pollutant degradation,  $K_i$  is the saturation constant,  $C_a$  is the concentration of the pollutant,  $-dC_a/dt$  is the disappearance rate of the pollutant, and  $n$  is the model fitting constant.

When TN is the sole nitrogenous source, the system is considered to be a non-inhibited system. As such, Monod's proposed kinetic model (Equation (3)) for non-inhibited systems, is deemed suitable to model such systems:

$$-\frac{dC_a}{dt} = \frac{V_m * C_a}{K_i + C_a} \quad (3)$$

where  $V_m$ , is the maximum specific degradation rate of the pollutant.

Haldane [13] also represented pollutant degradation kinetics using a model as shown in Equation (4):

$$-\frac{dC_a}{dt} = \frac{V_m C_a}{C_a + \frac{C_a^2}{K_i}} \quad (4)$$

Due to the possibility of inhibition of SNaD by  $\text{CN}^-$ , a model (Andrew's model) representing the kinetics of a primary pollutants' degradation in which a secondary inhibitory pollutant is present, was deemed necessary to use, as presented in Equation (5) [13]:

$$\frac{dC_a}{dt} = -V_m \left[ 1 - \left( \frac{K_i}{C_a} \right) \right] \left[ 1 + \left( \frac{C_a}{K_s} \right) \right] \quad (5)$$

where  $K_s$  is a secondary pollutants' inhibition constant.

## 2.6. Regression of Experimental Data and Estimation of Model Kinetic Parameters

Mathematical models describing  $\text{CN}^-$  and  $\text{NH}_4\text{-N}$  accumulation and degradation were fitted to the experimental data generated. Additionally, the models describing  $\text{NH}_4\text{-N}$  degradation with pollutant inhibition were also fitted into  $\text{NH}_4\text{-N}$  accumulation and accumulation experimental data. A nonlinear regression function in the Polymath 6.0 software was used for simulations, thus the generation of simulation data (using estimated kinetic parameters) that was compared to experimental data.

## 2.7. Data Handling and Kinetic Parameters

The data were computed and analyzed using Microsoft Excel v2016. The mean was determined using Equation (6); Moreover, Polymath 6.0 was used to estimate kinetic parameters in Equations (1), (4) and (6). The data obtained from polymath was plotted using Microsoft Excel v2016:

$$\text{Mean} = \frac{\sum X}{n} \quad (6)$$

where  $\sum X$  is the sum of the data points, while  $n$  is the number of experimental experiments conducted.

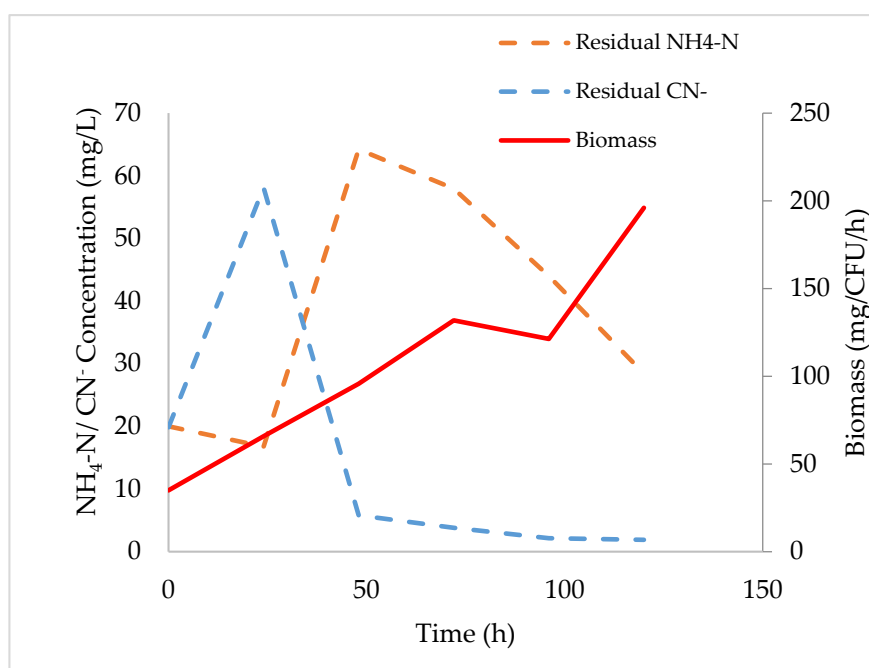
## 3. Results and Discussion

### 3.1. Identification of Bacterial Isolate

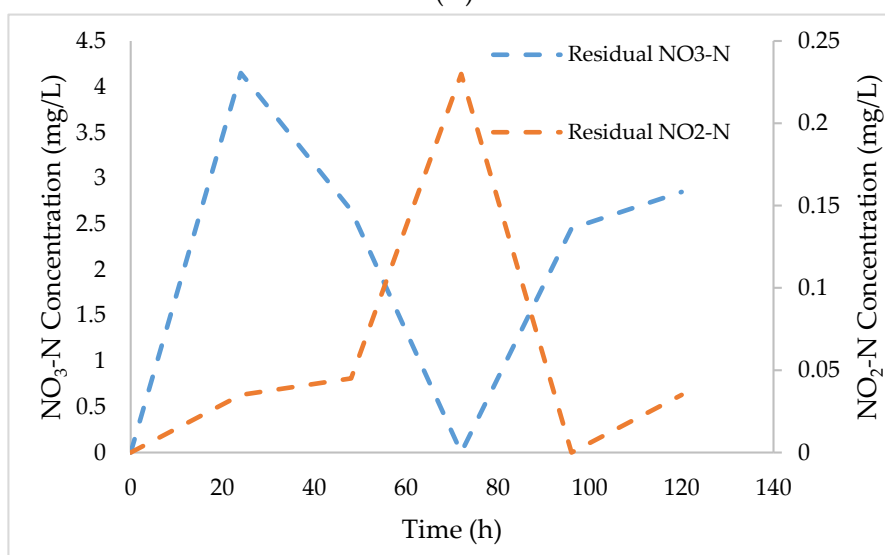
The  $\text{CN}^-$  resistant bacterial strain was characterized by sequencing 16sRNA using the universal primers 27F and 1492R to amplify the target region. The results were obtained by a BLAST search. The sequence on NCBI indicated that the isolated bacteria was *Acinetobacter courvalinii*, accession number AB602910.1/NR\_148843.1.

### 3.2. Degradation Kinetics of Cyanide and $\text{NH}_4\text{-N}$

An experiment was conducted to investigate the growth of *A. courvalinii* under  $\text{CN}^-$  conditions, subsequent to  $\text{CN}^-$  and TN biodegradation studies by the isolate. The growth of *A. courvalinii* was shown not to be affected by  $\text{CN}^-$  concentration of up to 20 mg  $\text{CN}^-/\text{L}$ ; therefore, it was selected for the assessment of its ability to perform SNaD under cyanogenic conditions. The isolate was found to possess a special ability of sequential utilization of  $\text{CN}^-$  and TN by exploiting its multi phased growth attributes, by initially utilizing of  $\text{CN}^-$  and subsequently,  $\text{NH}_4\text{-N}$ , which was evident by the appearance of a secondary logarithmic phase as seen in Figure 1A.



(A)



(B)

**Figure 1.** Biodegradation kinetics of  $\text{NH}_4\text{-N}$  and  $\text{CN}^-$  by *Acinetobacter courvalinii*. (A): Growth of *Acinetobacter courvalinii*, sequential degradation of  $\text{CN}^-$  and  $\text{NH}_4\text{-N}$ . (B):  $\text{NO}_2\text{-N}$  and  $\text{NO}_3\text{-N}$  accumulation and degradation.

Figure 1A, demonstrates that *A. courvalinii* utilized  $\text{CN}^-$  primarily, from a concentration of 20 mg  $\text{CN}^-/\text{L}$  to 5.8 mg  $\text{CN}^-/\text{L}$  followed by  $\text{NH}_4\text{-N}$ . The rate of degradation for both  $\text{CN}^-$  and  $\text{NH}_4\text{-N}$  was 2.2 mg  $\text{CN}^-/\text{L}/\text{h}$  and 0.40 mg  $\text{NH}_4\text{-N}/\text{L}/\text{h}$ , respectively. Moreover, a cyanide-degrading consortium was also assessed (Figure S1 Supplementary file A) as it was having similar attributes to the isolate used in this study; albeit, due to a large percentage of organisms within the consortium being identified as unknown (Figure S2 Supplementary file A), the results were not included nor discussed herein. Overall, an increase of  $\text{CN}^-$  in the first 24 h was observed, with a subsequent  $\text{CN}^-$  decrease from 58.1 mg  $\text{CN}^-/\text{L}$  to 5.8 mg  $\text{CN}^-/\text{L}$ , being observed. The initial increase in  $\text{CN}^-$  was associated with the activation of the ANR cascade which result in the production of HCN and denitrification enzymes (NAR, NIR, NOR, and  $\text{N}_2\text{OR}$ ) Figure 1A.

Arai et al. [14] reported the regulation of ANR cascade for transcription of denitrification enzymes resulting in the production of HCN by *Pseudomonas aeruginosa*. Moreover, the Pseudomonadaceae have been reported to possess the aerobic denitrification capability needed in the aiding and furtherance of SNaD [15]. *A. courvalinii* exhibited similar characteristics to those of *Pseudomonas sp.* Mpongwana et al. [10] also reported an increase in  $\text{CN}^-$  concentration during the expression of denitrification enzymes. For this study, a decrease in  $\text{NH}_4\text{-N}$  from 64.2 to 28.4 mg  $\text{NH}_4\text{-N}/\text{L}$  was observed, indicating an initiation of nitrification from the threshold limit of 5.8 mg  $\text{CN}^-/\text{L}$  Figure 1A. This indicated that a concentration of 5.8 mg  $\text{CN}^-/\text{L}$  did not completely inhibit nitrification; albeit, this concentration is above the threshold concentration of  $\text{CN}^-$  known to completely inhibit nitrification reaction [6]. Kim et al. [16] reported the complete inhibition of nitrification by 1 mg  $\text{CN}^-/\text{L}$ . The inhibition is largely associated with enzyme redundancy, non-production and deactivation.

The NAR which is activated during the regulation of ANR is a significant enzyme that aid in aerobic respiration; thus, converting  $\text{NO}_3\text{-N}$  back into  $\text{NO}_2\text{-N}$  during aerobic denitrification [17]. The increase of  $\text{CN}^-$  during the experiment, confirmed the ability of the *A. courvalinii* to induce ANR advocated for its ability to carry out SNaD. Minute accumulation of  $\text{NO}_2\text{-N}$  was observed compared to  $\text{NO}_3\text{-N}$  which was produced in significant quantities in the first 24 h of the experiments (Figure 1B). This was deemed normal as some studies have reported that  $\text{NO}_2\text{-N}$  accumulate in insignificant quantities during SNaD [18]. The  $\text{NO}_2\text{-N}$  increase between 48–72 h, was associated with the conversion of  $\text{NO}_3\text{-N}$  to  $\text{NO}_2\text{-N}$  catalysed by NAR during aerobic respiration culminating in the distinct feature of SNaD, a phenomena also supported by the observed decrease in  $\text{NO}_3\text{-N}$  between 24 and 72 h which corresponded with the increase of  $\text{NO}_2\text{-N}$ , confirming the ability of *A. courvalinii* to carry-out aerobic respiration thus performing SNaD.

A multi-phased growth, as observed in Figure 1A, confirmed multiple distinct dual lag phases with a stationery phase being observed between 72–96 h. This stationery phase was associated with biomass switching utilization from one nitrogenous source to another, i.e., from using  $\text{CN}^-$  to  $\text{NH}_4\text{-N}$ . The first lag phase from 0–72 h was linked with the isolates' growth as a result of  $\text{CN}^-$  presence, using it as a source of nitrogen, while the second lag phase from 96–120 h was linked with the growth of *A. courvalinii* as a result of  $\text{NH}_4\text{-N}$  consumption and/or removal, with growth rate being 1.35 and 3.12  $\text{h}^{-1}$  for first and second growth phases, respectively. This indicated that *A. courvalinii* grows well when supported by less toxic nitrogenous source ( $\text{NH}_4\text{-N}$ ) than when growing in a inhibitory toxicant ( $\text{CN}^-$ ) even if it's a nitrogenous source which can be utilized by the organism. However, the rate of  $\text{NH}_4\text{-N}$  removal was low thus, optimization studies are needed, in order to increase the nitrification efficiency, which is the initial step in SNaD. Subsequent to the monitoring of TN and  $\text{CN}^-$  removal, five models were used to assess their predictive ability of SNaD under  $\text{CN}^-$  conditions, with kinetic parameters in each model being determined.

### 3.3. Model Parameter Determination and Statistical Analysis

The predictive capability of the three models on  $\text{NH}_4\text{-N}$  degradation was analyzed. This was done by simulating the predicted model data in comparison to experimental data and also by plotting parity plots to assess the relationship between predicted data with the observed experimental values.



The selected models included the Rate law, Haldane and Andrew's models. The experimental data was fitted into the models to estimate kinetic constant in each model, using Polymath 6.0 software. The Rate law and Haldane models adequately described the experimental data of the nitrification step with a determination coefficient ( $R^2$ ) of 0.91 and 0.92, respectively (Table 1).

**Table 1.** Estimated kinetic parameter values for the models for  $\text{NH}_4\text{-N}$  degradation, a rate limiting step in nitrification.

Values of Kinetic Parameters ( $\pm 95\%$ Confidence Interval)						
Model	$V_m$ ( $\text{h}^{-1}$ )	$K_i$ ( $\text{mgL}^{-1}$ )	$K_s$ ( $\text{mgL}^{-1}$ )	$n$ (-)	$R^2$	Variance
Rate law $-\frac{dC_a}{dt} = r = K_i C_a^n$	-	0.0000629	-	2.27	0.91	0.02
Haldane $-\frac{dC_a}{dt} = \frac{V_m C_a}{C_a + \frac{C_a^2}{K_i}}$	0.45	23.94	-	-	0.92	0.02
Model with Substrate Inhibition						
Andrews $\frac{dC_a}{dt} = -V_m [1 - (\frac{K_i}{C_a})] [1 + (\frac{C_a}{K_s})]$	0.36	27.54	13.22	-	0.94	0.02

Equations (2)–(6) were obtained from Annuar et al. [13].

Furthermore, the adjusted determination coefficient (Adj  $R^2$ ) was 0.89 and 0.89 respectively, with such a high Adj  $R^2$  signifying a high significance, thus suitability of the estimated model kinetic constants. Furthermore, the variance was 0.015 and 0.016 for the generic rate law and the Haldane model, respectively. This variance is very low and is evidence that the predicted (modelled) values generated using estimated kinetic parameters did not differ much from experimental data. Similarly, Andrews model generated data with substrate inhibition was also compared to experimental data. The model gave a better fit with a correlation coefficient of 0.94 and a linear correlation efficient of 0.98 and an Adj  $R^2$  0.90.

The average standard deviations were compared for the selection of the better predicting model for  $\text{NH}_4\text{-N}$  degradation as a limiting step, with standard deviation of Haldane, Rate law and Andrew's model being 0.041, 0.043, and 0.036, respectively. However, for the selection of the model that is adequate in predicting multiple nitrogenous pollutants ( $\text{CN}^-$ ,  $\text{NH}_4\text{-N}$ ,  $\text{NO}_2\text{-N}$  and  $\text{NO}_3\text{-N}$ ) removal, the prediction ability of the model towards  $\text{CN}^-$  degradation needed to be considered. The parity plot indicated a satisfactory correlation between the experimental rate of  $\text{NH}_4\text{-N}$  degradation and the predicted rates with  $R^2$  being 0.96, 0.92, and 0.94 for Rate law, Haldane and Andrew's model respectively.

Moreover, the variance for Andrews's model also proved the significance of the model with variance being 0.015. This variance was minute which indicated that there was a negligible difference between the model and experimental data (see Figure 2 and Table 2). Monod and Moser models were also assessed for their predictive ability of  $\text{NH}_4\text{-N}$  (Figure S3 and Table S1, Supplementary file A) and  $\text{CN}^-$  (Figure S4 and Table S2, Supplementary file A) degradation rates; however, they did not fit well into the experimental data.

**Table 2.** Estimated values of kinetic parameters for the models for  $\text{CN}^-$  degradation.

Values of Kinetic Parameter ( $\pm 95\%$ Confidence Interval)						
Model	$V_m$ ( $\text{h}^{-1}$ )	$K_i$ ( $\text{mgL}^{-1}$ )	$K_s$ ( $\text{mgL}^{-1}$ )	$n$ (-)	$R^2$	Variance
Rate law $-\frac{dC_a}{dt} = r = K_i C_a^n$	-	$3.33 \times 10^{-5}$	-	2.65	0.92	0.05
Haldane $\frac{dC_a}{dt} = \frac{V_m C_a}{C_a + \frac{C_a^2}{K_i}}$	0.36	11.36	-	-	0.95	365.43

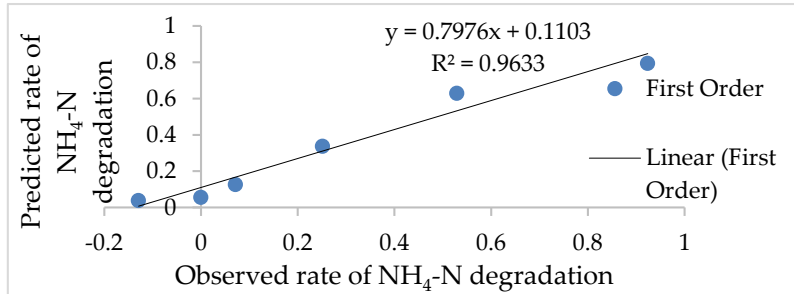
**Model**

Rate law

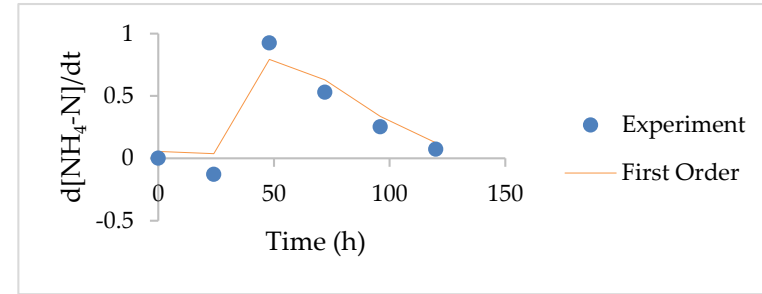
$$-\frac{dC_a}{dt} = r$$

$$= V_m C_a^n$$

**Parity Plots**



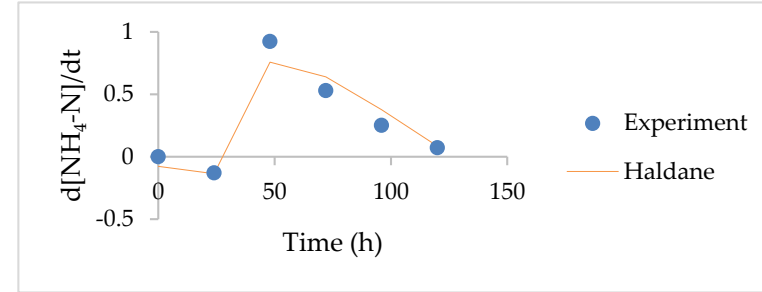
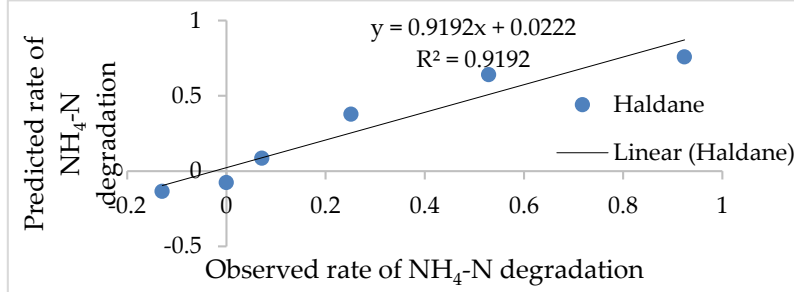
**Assimilation of Models into Experimental Data**



Haldane

$$\frac{dC_a}{dt}$$

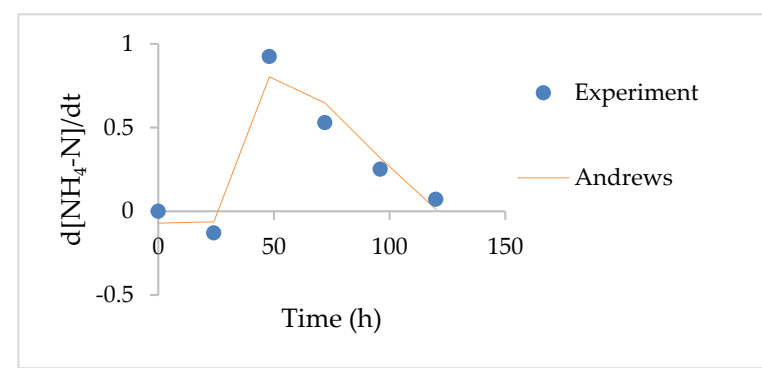
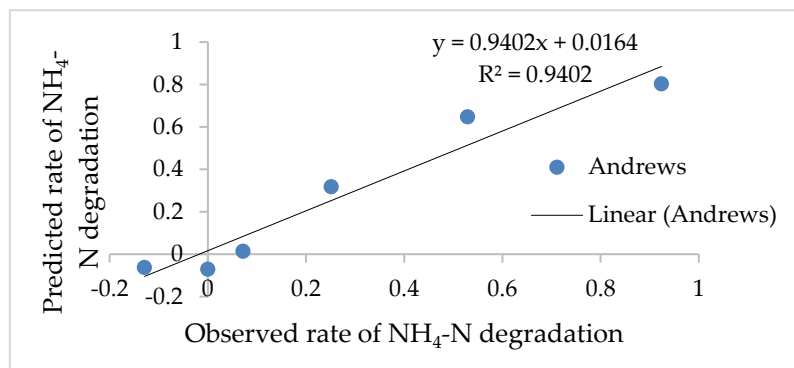
$$= \frac{V_m C_a}{C_a + \frac{C_a^2}{K_i}}$$



Andrews

$$\frac{dC_a}{dt}$$

$$= -V_m \left[ 1 - \frac{K_i}{C_a} \right] \left[ 1 + \frac{C_a}{K_s} \right]$$



**Figure 2.** Parity plots of predicted values versus experimental values. Assimilations of the model data into NH<sub>4</sub>-N degradation experimental data (Rate law, Haldane, and Andrew).



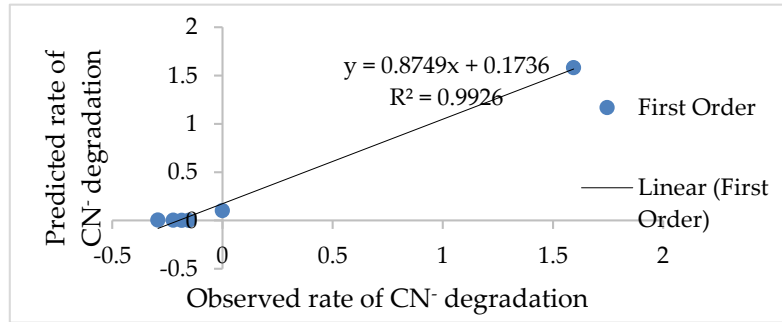
**Model**

Rate law

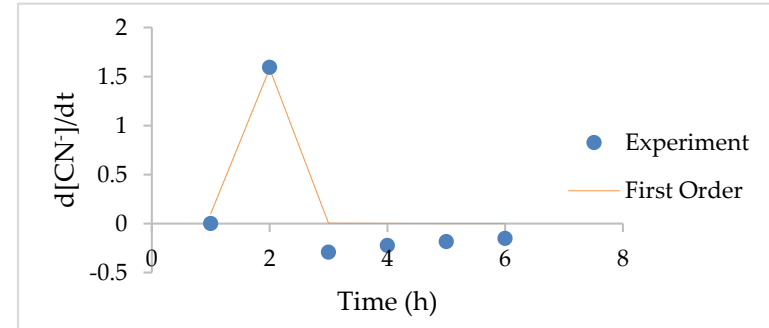
$$-\frac{dC_a}{dt} = r$$

$$= V_m C_a^n$$

**Parity Plots**

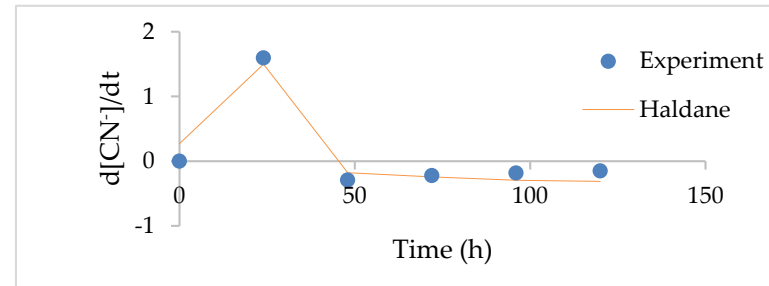
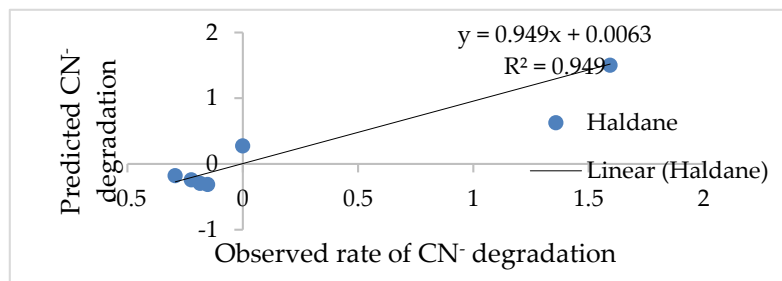


**Assimilation of Models into Experimental Data**



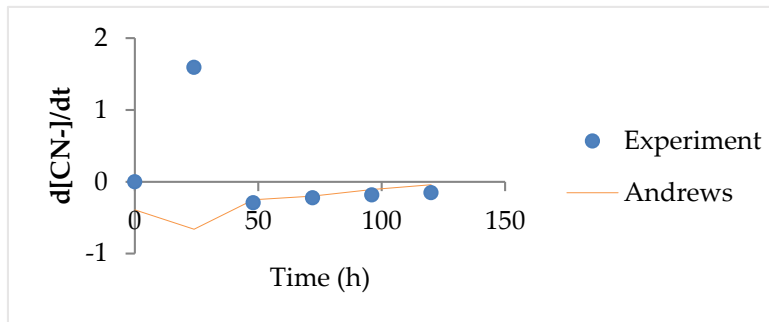
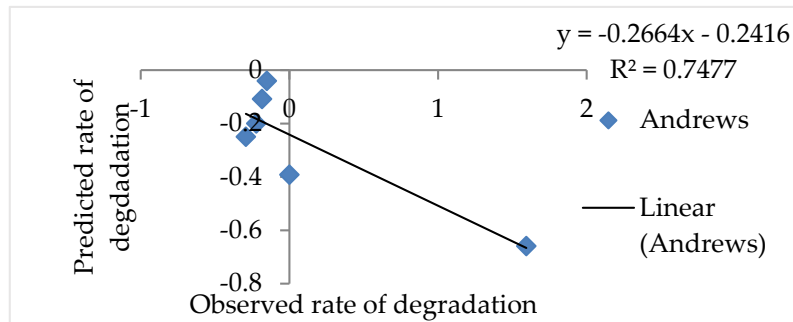
Haldane

$$\frac{dC_a}{dt} = \frac{V_m C_a}{C_a + \frac{C_a^2}{K_i}}$$



Andrews

$$\frac{dC_a}{dt} = -V_m \left[ 1 - \frac{K_i}{C_a} \right] \left[ 1 + \frac{C_a}{K_s} \right]$$



**Figure 3.** Parity plots of predicted values versus experimental values. Assimilations of the model data into CN<sup>-</sup> degradation experimental data (Rate law, Haldane, and Andrews).

Overall, the models used and reported in this research also fitted the  $\text{CN}^-$  degradation data well (Figure 3). The models that gave a better fit were the rate law ( $R^2 = 0.92$ ,  $\text{Adj } R^2 = 0.90$ , variance = 0.052 and standard deviation = 0.076) and Haldane model ( $R^2 = 0.95$ ,  $\text{adj } R^2 = 0.94$ , variance = 0.034 and standard deviation = 0.061)—see Table 3. Andrew models' had a poor prediction of  $\text{CN}^-$  degradation with ( $R^2 = -0.99$ ,  $\text{adj } R^2 = -2.31$ , variance = 1.75, and standard deviation = 0.38). This indicated that  $\text{CN}^-$  degradation was not inhibited by the presence of  $\text{NH}_4\text{-N}$ , as some organism would rather alternatively use the less inhibitory pollutant; although, inhibitory compound biodegradation might be a favorable alternative. Andrew's model was developed to predict substrate utilization in systems with substrate inhibition, thus the models' inability to model  $\text{CN}^-$  removal.

**Table 3.** Kinetic parameters obtained from different studies assessing nitrification and aerobic denitrification.

Model	Kinetic Parameters					Reference
	$V_m$	$K_s$	$K_i$	$n$		
Haldane	0.323	9.65	152.40	-	[19]	SNaD under high phenol concentrations using A strain capable of phenol degradation (Haldane model with substrate inhibition)
	0.45	-	23.94	-	This study	SNaD in $\text{CN}^-$ (Haldane model without substrate inhibition)
Rate law	-	-	0.047	1	[20]	Degradation of ammonia nitrogen under high phenol concentrations.
	-	-	$6.29 \times 10^{-5}$	2.27	This study	SNaD in $\text{CN}^-$
Andrews	0.0485	28.63	24.284	-	[20]	Denitrification with nitrate inhibition
	0.36	13.22	27.54	-	This study	SNaD in $\text{CN}^-$

$K_s$  is pollutant inhibition constant,  $K_i$  is the saturation constant,  $C_a$  is the concentration of the pollutant,  $n$  is the model fitting constant and  $V_m$ , is the maximum specific degradation rate of the pollutant.

Ge et al. [19] studied the kinetics of SNaD under high phenol concentrations using bacterial strains capable of phenol degradation, heterotrophic nitrification, and aerobic denitrification. Additionally, Vasiliadou et al. [20] also studied the kinetics of denitrification with nitrate inhibition. Additionally, Li et al. [21] also determined that the Haldane model predicted  $\text{CN}^-$  well with  $R^2$  being 0.99. These studies indicated the feasibility of SNaD, even under inhibitory pollutant loading. Moreover, the kinetic parameters obtained were comparable to those obtained for this study (Table 3).

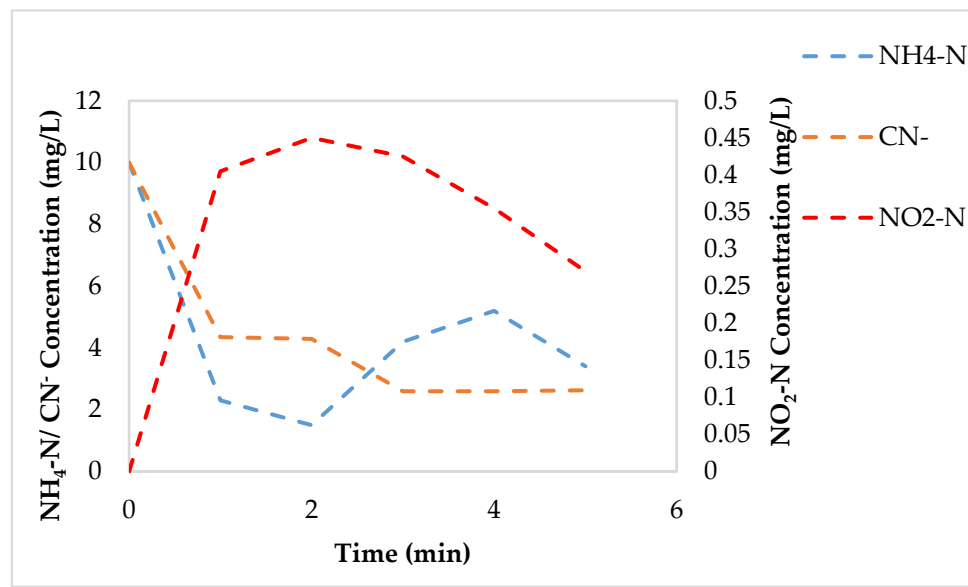
Overall, the variance and standard deviation of the model showed that all three models predicted  $\text{NH}_4\text{-N}$  degradation better as opposed to  $\text{CN}^-$  degradation. This was shown with the higher variances and standard deviation of  $\text{CN}^-$  degradation than those of  $\text{NH}_4\text{-N}$  degradation. Although, all three models adequately represented  $\text{NH}_4\text{-N}$  removal with high  $R^2$  and  $\text{adj } R^2$ , the rate law and Andrews models had higher average standard deviation and variance for predicted rate of  $\text{CN}^-$  degradation in comparison to actual experimental data (Figure 3); thus rendering unusable as candidate prediction models for removal systems with multiple nitrogenous pollutants.

Moreover, Haldanes' model was selected as a better predictor of  $\text{NH}_4\text{-N}$  removal under  $\text{CN}^-$  conditions. This decision was based on its standard deviation and the variance being the lowest for both  $\text{NH}_4\text{-N}$  and  $\text{CN}^-$  degradation, indicating that the predicted rate of  $\text{NH}_4\text{-N}$  and  $\text{CN}^-$  by Haldane had a minute deviation from the experimental data thus qualifying it as a better model to be used for multiple nitrogenous pollutants systems, especially, SNaD.

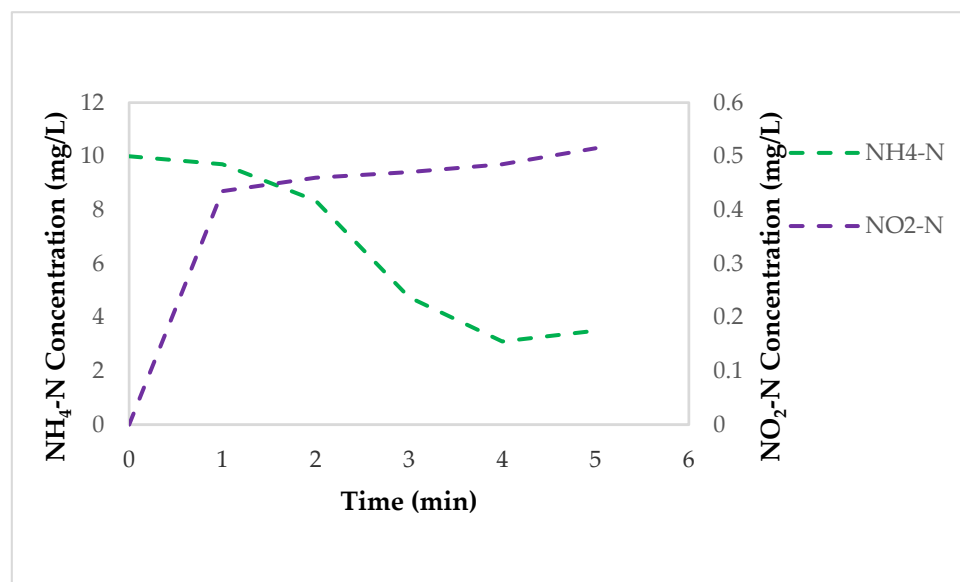
The result obtained in this study were consistent with those that were previously reported by Pradhan et al. [22] describing dual substrate kinetics of ammonia oxidation by Haldane model, with  $R^2 > 0.98$  and  $\text{adj } R^2 > 0.98$  and low standard errors (RMSE)  $< 0.61$ . Additionally, Wang et al. [23] reported a high correlation between Haldane prediction and experimental data with adjusted  $R^2$  (0.995),  $K_s$  ( $2.997 \pm 0.041$  mg/L) and  $K_i$  ( $64.736 \pm 0.023$  mg/L).

### 3.4. Effect of Cyanide on AMO, NaR, and NiR

Enzyme inhibition can occur in different ways such as the binding of an inhibitor onto an active site or for an example a site of the AMO responsible for  $\text{NH}_4\text{-N}$  oxidation. The second inhibition mechanism can involve the removal of the Cu co-factor of AMO which in turn affects the activity of AMO [24]. To assess the effect of  $\text{CN}^-$  towards SNaD, enzyme extracts from *A. courvalinii* cultivated in batch cultures were used. The effect of  $\text{CN}^-$  towards the expression of  $\text{NH}_4\text{-N}$  (AMO),  $\text{NO}_3\text{-N}$  (NaR) and  $\text{NO}_2\text{-N}$  (NiR) oxidizing enzymes was evaluated (Figure 4A).



(A)



(B)

**Figure 4.** The activity of  $\text{NH}_4\text{-N}$ ,  $\text{NO}_3\text{-N}$  and  $\text{NO}_2\text{-N}$  oxidizing enzymes and  $\text{CN}^-$  degrading enzyme. (A): Effect of  $\text{CN}^-$  on the induction of  $\text{NH}_4\text{-N}$ ,  $\text{NO}_3\text{-N}$  and  $\text{NO}_2\text{-N}$  oxidizing enzymes by *A. courvalinii*. (B): Effect of  $\text{CN}^-$  on free cell  $\text{NH}_4\text{-N}$ ,  $\text{NO}_3\text{-N}$  and  $\text{NO}_2\text{-N}$  oxidizing enzymes.

The activity and presence of AMO, NaR, and NiR was conducted using cell-free extracts by the addition of the enzyme solution into solutions of  $\text{NH}_4\text{-N}$ . The results revealed that *A. courvalinii*

was able to express AMO, and not NaR and NiR; this was shown by the decrease of  $\text{NH}_4\text{-N}$  and the accumulation of  $\text{NO}_2\text{-N}$ ; however, there was minimal  $\text{NO}_2\text{-N}$  oxidation observed thus minimal  $\text{NO}_3\text{-N}$  formation and accumulation detected (see Figure 4B). This observation led to a hypothesis that  $\text{CN}^-$  inhibited the expression of  $\text{NO}_3\text{-N}$  and  $\text{NO}_2\text{-N}$  oxidizing enzymes or results in the excretion of non-active  $\text{NO}_3\text{-N}$  and  $\text{NO}_2\text{-N}$  oxidizing enzymes.

In addition, the competitive inhibition by the addition of  $\text{CN}^-$  to free cell extract was examined. This experiment aimed to determine the effect of  $\text{CN}^-$  on the expressed  $\text{NH}_4\text{-N}$ ,  $\text{NO}_3\text{-N}$ , and  $\text{NO}_2\text{-N}$  oxidizing enzymes, of which the outcomes indicated that the presence of  $\text{CN}^-$  did not have an effect on the  $\text{NH}_4\text{-N}$  reducing enzyme; albeit, a slow decrease of  $\text{NO}_2\text{-N}$  was observed which suggested the activation of denitrification. Additionally, no  $\text{NO}_3\text{-N}$  accumulation was observed which meant that *A. courvalinii* converted  $\text{NO}_2\text{-N}$  directly to  $\text{N}_2$ .

The activation of  $\text{NO}_2\text{-N}$  genes when  $\text{CN}^-$  was added to bacterial cultures, could be a confirmation that *A. courvalinii* expresses an ANR protein in response to the presence of  $\text{CN}^-$  as a protective mechanism for the cyanide-resistant bacteria used in this research in order to mitigate against the toxicity of the  $\text{CN}^-$ . Furthermore, the activation of this protein can lead to the induction of NAR, NIR, NOR and  $\text{N}_2\text{OR}$  although this was not confirmed in this study [1].

#### 4. Conclusions

The growth of *Acinetobacter courvalinii* accession number AB602910.1/NR\_148843.1 was not affected by  $\text{CN}^-$ . Furthermore, this microorganism was shown to carry-out SNaD under higher  $\text{CN}^-$  concentration than the threshold concentration which is known to completely inhibit SNaD. The predictive ability of the rate law, Haldane, and Andrew's models was assessed with results indicating that the rate law, Haldane, and Andrew's models were better models to predict  $\text{NH}_4\text{-N}$  removal as the initial step in SNaD, with high  $R^2$  and adj  $R^2$ ; thus, the evaluation of models ability to also predict  $\text{CN}^-$  degradation, with the standard deviation and variance being a criterion for selection of the better predicting model. The Haldane model was found to have the lowest standard deviation for both  $\text{CN}^-$  and  $\text{NH}_4\text{-N}$  removal among all models evaluated. Thus it's selection as a model that is suitable to predict the detoxification of TN in wastewater, using SNaD even under  $\text{CN}^-$  laden conditions.

The influence of  $\text{CN}^-$  on AMO, NaR, and NiR also showed that  $\text{CN}^-$  did not affect the expression and activity of  $\text{NH}_4\text{-N}$  oxidizing enzymes and the assumption was made that non-viable  $\text{NO}_3\text{-N}$  and  $\text{NO}_2\text{-N}$  reducing enzymes were expressed. This hypothesis comes from the observation of the slow decrease in  $\text{NO}_2\text{-N}$  after the addition of  $\text{CN}^-$  on crude enzyme extract assays, confirming the activity of  $\text{NO}_3\text{-N}$  reducing enzyme and activation of the denitrification pathway by the  $\text{CN}^-$ . Although *A. courvalinii* have been shown to be able to detoxify TN under  $\text{CN}^-$  conditions, its physico-chemical parameters still need to be investigated in order to optimize the degradation efficiency of isolate, *A. courvalinii*

**Supplementary Materials:** The following are available online at <http://www.mdpi.com/2076-3417/10/14/4823/s1>, Figure S1: Simultaneous nitrification and aerobic denitrification performed by cyanide degrading consortia under high cyanide conditions. Figure S2: Metagenomics report for the consortium. A: Kingdom classification. A: Phylum classification. C: Class classification. D: Order classification. E: Family classification. Figure S3: Parity plots of predicted values versus experimental values. Assimilations of the model data into  $\text{NH}_4\text{-N}$  degradation experimental data (Monod and Moser). Figure S4: Parity plots of predicted values versus experimental values. Assimilations of the model data into  $\text{CN}^-$  degradation experimental data (Monod, Moser and Andrews). Table S1: Estimated values of kinetic parameters for the models for  $\text{NH}_4\text{-N}$  degradation, a limiting step in nitrification. Table S2: Estimated values of kinetic parameters for the models for  $\text{CN}^-$  degradation, a limiting step in nitrification.

**Author Contributions:** Conceptualization, N.M.; Formal analysis, N.M., E.I.O., S.K.O.N., L.C.R. and B.S.C.; Methodology and investigation, N.M., C.D. and M.R.M.; Funding acquisition, S.K.O.N.; Investigation, N.M.; Project administration, S.K.O.N., B.S.C., L.C.R. and E.I.O.; Resources, S.K.O.N.; Supervision, S.K.O.N., B.S.C. and E.I.O.; Writing—original draft, N.M.; Data interpretation, review & editing, N.M., S.K.O.N., E.I.O., L.C.R. and B.S.C. All authors have read and agreed to the published version of the manuscript.

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**Conflicts of Interest:** The authors declare that there is no conflict of interest related to this study.

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